ABSTRACT
Large numbers of culverts are to be constructed in a hilly road for cross-drainage purpose for the safety and efficient functioning of the road. Optimum spacing of culverts is governed by the type of terrain and its steepness, road alignment, longitudinal slope of road, rainfall intensity and average width of catchment. An economic analysis is performed to determine the optimum spacing of culverts in between ridge and valley points of the road so that the total cost of culvert and drain is minimum. Hydrologic and hydraulic design considerations for finding design discharge and carrying capacity of culverts are discussed. Typical drawings for slab type and hume pipe culverts showing improved inlet and outlet transitions are presented.

Key Words: Culvert, Design, Hilly Terrain, Optimum Spacing, Transitions.

1 INTRODUCTION
Drainage of roads in both plain and hilly terrains is extremely important for improvement in riding quality, safety as well as increasing life span of a road. Although the cost of longitudinal drainage (leaving cost of bridges/culverts) varies from 1 to 2 percent of road cost, design of drainage is often neglected by the project authorities resulting in lot of problems e.g. damage to road, poor riding quality, skidding, hydro planning etc. Various objectives of road drainage are

- To remove storm water from road surface as rapidly as possible to avoid skidding, splashing, hydro planning etc.
- To ensure road safety and prevent traffic hazards
- To prevent inundation of road surface from run-off / flood water in flowing streams since road acts as a barrier to free run off movement that used to occur prior to road construction
- To ensure structural safety of road, bridges and culverts
- To maintain a healthy road, bridges and other cross-drainage works free from water congestion settlement of embankment causing pot holes, undulations etc.
- To reduce/minimize maintenance cost and longer life span of the road

Essential requirements of an ideal road drainage system are summarized below:

- Run-off from the catchment area should be disposed as quickly as feasible.
- Run-off water from both sides of the terrain (road in valleys) or from upstream side (in terrains with one side sloping) should be intercepted in a roadside drain so that run-off water moves to the cross-drainage system quickly and a continuity of flow is maintained.
• Road must have adequate cross-slope or camber as per Clause 5 of IRC, SP-42(1994) for quick disposal of storm water run-off laterally to the road side drain / drains.

• A minimum longitudinal grade of ½% should be provided to the road wherever possible for facilitating both surface and sub-surface drainage.

• Adequate size and numbers of cross-drainage structures (Bridges and culverts) should be provided to ensure safe and quick disposal of storm water.

• Intercepting drain, as in a hilly terrain sloping towards the road, should have adequate size and be connected properly with well designed culverts/bridges.

• In case width of terrain contributing flow to the drain is very high, intercepting drain at higher elevation should be provided.

• The drain should be connected to the cross drainage structures so designed that the water moves out without any objectionable heading up/afflux and there is no overtopping of road and the hydraulic structures.

• GSB/drainage layer should be provided for sub-surface drainage of percolating/seepage water as well as for intercepting capillary water.

This paper deals with the drainage requirement, planning and optimal spacing of culvers, hydrologic/hydraulic design of culverts in the hilly stretch of Buangpui – Lunglei state road in the state of Mizoram. Proper planning of drainage culverts (Mazumder and Poudel, 2002) in a hilly area like Mizoram and similar terrains in the North-East of India is a prerequisite for a healthy road free from traffic hazards as well as for durability of the road.

2 LOCATION OF CULVERTS IN THE HILLY STRETCH OF THE ROAD

Buangpui–Lunglei state road in Mizoram is a single lane state road mostly in the hilly terrain. It is proposed to widen it to ½ specifications. Fig. 1 shows the location of 170 existing drainage culverts (indicated by arrows) in the hilly stretch of the road from 128.525 km to 170.944 km having a length of 42.414 km. The average distance between consecutive culverts is about 250 m or in other words about 4 numbers of culverts are provided per km of road. In such a terrain with high rainfall intensity, perhaps more culverts should have been provided. In this stretch of road, there is only one bridge over river Tlwang and as such the culverts form the lifeline of the drainage system. Location and spacing of culverts are generally governed by three major factors, namely,

(a) Width of the catchment (i.e. the distance between the road and the terrain ridgeline normal to the road) contributing runoff towards the road

(b) Rainfall intensity in the catchment

(c) Longitudinal slope of the road

Culverts are to be provided at all valley points where the road crosses torrents for passing the storm water to the valley. In addition, the intermediate culverts are necessary in order to limit the size of the drains running parallel to the road at the foothill for intercepting run-off and disposing it to the valley side through the
drainage culverts. Too wide a drain along foothill will increase the cost of hill excavation besides destabilizing hill slope. Costly slope protection measures are to be adopted for stabilizing the hill slope. Usually Vee-shaped triangular open drains of depth varying from 30cm to 40cm with road-side slope (of the drain) not exceeding 3(H): 1(V) is recommended by hill-road manual (IRC-48,1998) to avoid traffic hazard. As such, the carrying capacity of the drain, depending on size and longitudinal slope of the drain (which is almost same as that of the road) is limited. If the spacing of intermediate culverts is too far, the drains will overflow, especially near outfall points and damage the road. In the built-up areas, however, covered trapezoidal concrete/boulder drains (IRC:SP-50,1999) have been provided in order to increase conveying capacity of the drain with a view to protect the built-up / habitated areas from run-off hazards.

3 BLOCKAGE OF DRAINS / CULVERTS AND DAMAGE TO ROAD SURFACE

Author visited the existing road and the adjoining drainage system from Buangpui to Lunglei. Most of the drains have been overflowing causing immense damage to the road surface as evident from photographs 1 and 2. It is noticed that the drains and culvert inlets are blocked due to deposition of stones and debris falling from hills, especially in areas susceptible to slip failure of hill face in the unstable regions, resulting in loss of drain and culvert capacity. Due to undersized culverts and their blockage by debris and jungles (photograph-3), choking of the drains, poor cross slope and excessive long slope of road, growth of jungles in the valley side curbs (there is hardly any maintenance), run-off water from the hills virtually move all along the road surface causing erosion of bituminous top surface and extensive damage to the road as evident from the photographs.

4. TYPE, SIZE, SPACING AND CARRYING CAPACITY OF CULVERTS

Majority of the existing culverts are made of Hume pipes (HP) of sizes varying from 60 cm to 100 cm. Box type concrete culverts are provided to augment culvert capacities wherever required (photograph-4). To ensure smooth and free flow, slab-type culverts with masonry abutments having spans varying from 2m to 5m are provided in all such locations where the discharge is very high and the torrents carry debris, gravels and boulders during flood season. As already mentioned earlier, average distance between consecutive culverts is about 250 m. With a view to examine whether the spacing is adequate or not, an economic study is made to determine the optimum spacing of the intermediate culverts, as discussed in the following paragraphs. Drainage capacity of culverts should be equal to or more than the incoming flow from the adjoining drains and the torrents discharging in to the culverts i.e. the total runoff generated from the catchment contributing
Fig.1 Culverts in the Hilly Stretch of Buangpui-Lunglei State Road in Mizoram
(Arrowheads Indicate Location of Culverts)

Hydraulic Design procedure of culverts are given in IRC-SP!3 (2004), AASHTO (1975), USBR(1968). Because of steep slope of culverts discharging in the valley (resulting in shooting supercritical free flow at outlet), most of the culverts are of inlet control types. Since top of culverts are to be below road crust, the culvert inverts at entry are to be lowered by providing catch pits of adequate depth to accommodate them. Water from the drains drops into the catch pit, heads up and then starts flowing through the culverts to dispose the design discharge when the head is maximum.

Discharging capacity \( Q_c \) of HP culverts under inlet control can be expressed as

\[
Q_c = C A \left(2gH_w\right)^{1/2}
\]

where \( C \) is the coefficient of discharge depending on whether the head \( (H_w) \) is measured above invert or from the center of conduit, head to depth ratio \( (Hw/D) \), \( D \) being the height of opening of the conduit at the inlet and the inlet geometry. \( A \) is the cross sectional area of flow of the conduit at entry in the plane of inlet headwall (for a HP culvert \( A = \left(\pi/4\right)D^2 \), \( g \) is acceleration due to gravity.

Depth of catch pits is found to vary from 2m to 4m, depending on terrain conditions, size of drain at its outfall and depth of culvert etc. It is noticed that many of the culverts are blocked at inlet since the catch pits are full of large size stones and debris carried by the drains as well as the torrents.
At many places, the blockage of inlet (photograph-3) has resulted in loss of carrying capacity of culverts, heading up of water level and overtopping of road resulting in damage to the road, inconvenience to traffic and slowing down of the vehicle speed. Inlet transition connecting the torrent with culvert has been modified to improve the carrying capacity and free movement of stones.

5. OPTIMUM SPACING OF CULVERTS
As stated earlier, if the distance between consecutive culverts is too large, size of drain will increase and hence its cost; but the total number of culverts will reduce and hence the total cost of culverts will be less. On the contrary, if the spacing is too small, the total number of culverts and culvert cost will be more but the size and cost of drain will reduce. An economic analysis is, therefore, made to examine at what spacing of culverts, the total cost of drain and culverts becomes minimum.
Total cost of drain and culvert is computed per kilometre of road. A fixed size of 1m diameter HP culvert is considered for the economic analysis. If $S$ is the assumed spacing of culverts in meter, number of culverts of 1m diameter shall be $1000/S$ per km of road.

As stated earlier, the three most important parameters which govern the size and cost of drain are (i) width and steepness of the catchment (i.e. the distance between the road and the ridgeline) contributing runoff towards the road, (ii) rainfall intensity in the catchment and (iii) longitudinal slope of the road/drain.

For any assumed spacing of culverts, the size of drain is found by computing run-off from the catchment contributing flow into the culvert. The maximum flow computed from the design rainfall intensity (on the basis of design storm of 25 year return period) and the catchment area is determined by using Rational formula:

$$Q = 0.028 f P I c A$$

where $Q$ is the design discharge in cumec, $f$ is spread factor, $P$ is run-off coefficient depending on permeability and slope of catchment, $I_c$ is design rainfall intensity (corresponding to time of concentration) in cm/hr and $A$ is the catchment area in hectare. Size of drain to carry the design discharge ($Q$) is determined by using Manning’s formula:

$$Q_c = 1/n (AR^{2/3} S_0^{1/2})$$

where $Q_c$ is the carrying capacity of drain in cumec, $n$ is rugosity coefficient, $A$ is the cross-sectional area of flow in the drain in m$^2$, $R$ is hydraulic mean depth in m and $S_0$ is the longitudinal slope of the drain. Drain size was fixed so that $Q = Q_c$. Knowing the drain size, cost of stone pitched drain - both Vee-type and trapezoidal covered drains (depending on spacing of culverts and size of drain) is computed. Cost of $1000/S$ number of H.P. culverts of 1m diameter along with cost of catch pit, inlet and outlet transitions etc. is computed. Total cost of drain and culvert per kilometre of road is found by adding up the cost of drain with cost of culverts. The total cost so found is plotted against spacing of culverts assumed. Fig.2 is one of the typical plots showing the cost of drain, cost of culvert and total cost of drain and culvert against different assumed spacing of culverts for a 50 m width of catchment and a road slope of 3%. Optimum spacing of culverts corresponding to minimum total cost is found to be 170m. Similar curves are plotted for 70m and 125m width of catchment for 7 different road slopes varying from 1% to 7%. Fig.3 shows a typical plot of total cost of drain and culvert against different spacing of culverts for 7 different slopes of road varying from 1% to 7%. Similar plots are made for 70m and 125m widths of catchment. The locus of optimum spacing of culverts corresponding to minimum total cost is indicated by dashed line in Fig.3. A master table is prepared from Fig.3 and similar figures for other widths of catchment giving the optimum spacing of culverts, as illustrated in table-1.

Table-1 shows that optimum spacing of culverts increase with increases in road slope for a given width of catchment and decreases with increase in width of catchment for any given slope of road. It may be
mentioned that table-1 and the figures-2 and 3 are applicable only for the design rainfall of 25 year return period found from iso-pluvials for the Buangpui-Lunglei region, subzone:2 (c) covering Mizoram state (CWC-2c)

6 IMPROVED INLET AND OUTLET TRANSITIONS FOR CULVERTS

During the site investigations and field data collection for the existing drains and culverts, it has been observed that the inlet and outlet transitions of the Box/HP culverts are not properly designed. Inlet catch pits where the drains drop abruptly are mostly filled with stones and debris resulting in substantial loss of head causing rise in head water elevation, overflow and damage to the road. Similarly, the outlets are found to end abruptly without any transition for diffusion of high velocity jet flow with high discharge intensity coming out of the culverts. There is hardly any downstream protection resulting in scouring of ground, lack of safety to the culvert and endangering the hill slope stability downstream of the culvert. Although debris can be removed manually, it is difficult to lift the heavy stones from deep catch pits. It is also noticed that during the non-monsoon season when most of the torrents run dry, the local people collect subsurface ground water by driving bamboo pieces inside the hill adjoining the torrents upstream of the culvert with great difficulty.

Keeping all the above points in view, the inlet and outlet transitions are modified as shown in Fig. 4 (slab culverts) and Fig.5 (H.P/Box culverts). Since the road is to be widened from one lane to one and half lane by excavating rocks in the hill side upstream of culvert, the existing catch pits at inlets have to be filled in and new inlets are to be built. Instead of providing one deep catch pit, it is divided into two shallow pits in the improved design of inlet. The upper pit is provided with a concrete overflow type weir to intercept heavy stones moving with flow while the lower pit will receive comparatively clear water with sand and smaller stones which will easily move out of the culverts. The upper pit with the front weir and side walls is so designed that it forms a wide pool of water and act as temporary storage for the heavier stones and water which can be easily collected by the local people for domestic use.

At the outlet, floor is stepped and bed is paved with stone pitching in between the flaring side walls for energy dissipation and flow diffusion. The downstream protection works is to be extended up to a distance so that the flow velocity and discharge intensity at the exit of protection works is sufficiently reduced without causing any objectionable scour downstream. It is, however, necessary to periodically remove the stones and debris from the upper pit for its efficient functioning. Similarly, the downstream protection works may need repair after the monsoon flood.

SUMMARY AND CONCLUSION

Buangpui-Lunglei state road in Mizoram is proposed to be widened from existing single lane to ½ specifications lane. The road is badly damaged due to inadequate number of drainage culverts most of which are found to be choked due to stones and debris deposited in the deep catch pit at entry to the culverts.
Capacity of the culverts is substantially reduced due to growth of jungles at the inlets. An economic study for determining optimum spacing of drainage culverts has been carried out. It is found that the optimum spacing decreases with increase in width of catchment for any given slope and increases with increase in road slope for any given width of catchment. Typical cases of optimum spacing corresponding to minimum total cost of culverts and drains per kilometer of road are illustrated figures 2 and 3 and are summarized in table-1- applicable for the design rainfall intensity in the Buangpui-Lunglei area in Mizoram state. In order to overcome the various difficulties, an improved design of inlet and outlet transitions as illustrated in Figures 4 and 5 are recommended for efficient functioning of the drainage culverts for this road.
Fig. 2 Showing Cost of Drain and Culvert and Total Cost against Spacing indicating Optimum Spacing of Culvert for 50m Width of Catchment and 3% Road Slope

Fig. 3 Showing total Cost of Culvert and drain against Spacing indicating Optimum Spacing of Culvert for 50m Width of Catchment and Road Slope varying from 1% to 7%
Fig. 4 Showing Improved Inlet and Outlet Transitions for Slab Culverts
Table 1: Optimum Spacing of Culverts for Different Slopes & Width of Catchment

<table>
<thead>
<tr>
<th>Slopes (%)</th>
<th>Widths of Catchment (m)</th>
<th>50m</th>
<th>70m</th>
<th>125m</th>
</tr>
</thead>
<tbody>
<tr>
<td></td>
<td>50m</td>
<td>70m</td>
<td>125m</td>
<td></td>
</tr>
<tr>
<td>1</td>
<td>130</td>
<td>125</td>
<td>100</td>
<td></td>
</tr>
<tr>
<td>2</td>
<td>150</td>
<td>145</td>
<td>125</td>
<td></td>
</tr>
<tr>
<td>3</td>
<td>170</td>
<td>160</td>
<td>150</td>
<td></td>
</tr>
<tr>
<td>4</td>
<td>180</td>
<td>170</td>
<td>160</td>
<td></td>
</tr>
<tr>
<td>5</td>
<td>190</td>
<td>180</td>
<td>170</td>
<td></td>
</tr>
<tr>
<td>6</td>
<td>195</td>
<td>190</td>
<td>180</td>
<td></td>
</tr>
<tr>
<td>7</td>
<td>200</td>
<td>195</td>
<td>190</td>
<td></td>
</tr>
</tbody>
</table>
ACKNOWLEDGEMENT

Author wishes to convey his gratitude to M/S ICT Pvt. Ltd, New Delhi, for all the co-operation and help received for writing the paper.

REFERENCES


CWC-2 (c) ‘Flood Estimation Report for Barak and Others’ Sub-zone (2c )’ – A Joint Work of Central Water Commission (CWC), Indian Meteorological Deptt (IMD), Research, Design and Standards Organisation (RDSO) and Ministry of Shipping, Highways & Road Transport (MOSHRT), pub. by Directorate of Hydrology, CWC, New Delhi.


FHWA ‘Hydraulic Design of Highway Culverts’ Hydraulic Design Series No.5 (HDS5), Federal Highways Administration, USA

HEC-12 (1984), ‘Drainage for Highway Pavements’ pub. by U.S.Federal Highway Administration,


